

CFD Simulation of Cavitation in an Internal Gear Pump



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Introduction into internal gear pumps:

- Positive displacement machine:
 - Liquid is displaced between large exterior gear and small interior gear
 - Crescent divides low and high pressure side (as a seal)
 - Suction / discharge can be in radial or axial direction
- Advantages:
 - Liquids with wide viscosity range, even with particles
 - Discharge rate almost independent of pressure conditions







- Inner rotor:
 - 13 teeth
 - 24.4 mm outer diameter
- Outer rotor:
 - 19 teeth
 - 34.0 mm outer diameter
- 4.77 mm eccentricity
- 16.1 mm thickness
- Suction / discharge in axial direction





- Stationary part:
 - suction and pressure port with
 6 mm diameter and
 10 mm length





- Stationary part:
 - suction and pressure port with
 6 mm diameter and
 10 mm length
 - axial interfaces between ports and rotors
 - crescent to separate chambers





- Radial clearances:
 - internal gear to crescent: 65 µm
 - external gear to crescent: 50 μm
 - between gears: >100 µm (no contact point)
- Axial clearances can be included





Mesh:

- Stationary part:
 - ANSYS Meshing for hybrid mesh
 - 800,000 elements, 280,000 nodes
- Rotating parts:
 - TwinMesh for hexahedral meshes
 - 20 radial x 30 axial x 46 per tooth
 - internal gear 360,000 elements
 - external gear 520,000 elements





What is TwinMesh?

- Challenges in geometry
 - two intermeshing gears
 - size-changing chambers
 - very small clearances (5-50 μm)
- Challenges in flow modelling:
 - transient with mesh deformation
 - strong gradients and high velocities in small gaps

Challenges in mesh generation:

- high mesh quality
- constant mesh topology to avoid interpolation
- ensure continuous mesh motion
- small manual effort, but flexible

SpaceClaim / DesignModeler





Mesh:

- Grid interfaces
 - GGI between rotating and stationary parts





Mesh:

- Grid interfaces
 - GGI between rotating and stationary parts
 - GGI between rotating parts





Simulation setup:

- Single-phase flow: water at 25°C
- transient simulation with 500 to 10,000 rpm for internal gear
- 20 to 200 meshes per tooth
- SST turbulence model
- suction and pressure side as opening with total pressures of 1 bar and 10 bar
- no-slip walls
- approx. 3 hours on 8 cores for 40 time steps (one tooth)





Single-phase results:

- Pressure:
 - linear pressure increase at crescent
 - sharp pressure increase between gears
 - pressure peaks <1 bar and >10 bar in intermeshing region



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Single-phase results:

- Velocity:
 - fluid is displaced in chambers towards pressure side (rotational speed < 5 m/s)
 - backflow in radial clearances with >10 m/s, in intermeshing clearance with >30 m/s





Single-phase results:

• Time-resolved results (40 meshes per tooth)



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Single-phase results:

• Time-averaged results



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Results with cavitation:

• Time-averaged results





Results with cavitation:

• Time-resolved results (40 meshes per tooth)



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Results with cavitation:

- Animation for 4000 rpm:
 - vapor is generated where teeth separate
 - vapor condensates before crescent
 - only water is displaced along crescent
 - same massflow as singlephase case



>10% vapor volume fraction

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Results with cavitation:

- Animation for 8000 rpm:
 - vapor is generated where teeth separate
 - vapor stays at internal gear along crescent
 - water and vapor are displaced along crescent
 - less massflow as singlephase case



>10% vapor volume fraction

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Cavitation with Rayleigh-Plesset model:

- Homogeneous Euler-Euler multi-phase simulation
 - Condensation if p>p_v:
 - Evaporation if $p < p_v$: $\dot{m}_{fg} = F \frac{3r_{nuc}(1-r_g)\rho_g}{R_{nuc}} \sqrt{\frac{2}{3} \frac{|p_v - p|}{\rho_f}}$

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- accelerates convergence and mass conservation, but less stable
- cavitation finite pcoef factor=0 (old behaviour: 1)
- Combination with "Cavitation Pressure Coefficient Factor" possible

 $\dot{m}_{fg} = F \frac{3 r_g \rho_g}{R_B} \sqrt{\frac{2}{3}} \frac{|p_v - p|}{\rho_f}$

- But pressure in simulation still drops below p_v , even below 0 Pa!
 - model coefficients calibrated on hydrofoils and ship propellers
 - second order term and surface tension neglected in derivation of RP model
 - vapor assumed incompressible at saturation pressure \rightarrow ideal gas law
 - outgassing of dissolved gas neglected \rightarrow full cavitation model

$$p_v = 3574 \text{ Pa}$$

$$R_{nuc} = R_B = 1 \mu m$$

$$r_{nuc} = 5E-4$$

$$F_{vap} = 50$$

$$F_{cond} = 0.01$$





Increasing rotational speed (periodic state for each rpm):

ANSYS R18.2



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Summary and conclusions

- TwinMesh and ANSYS CFD
 - simulation of PD machines
 - high quality meshing, easy setup
- Simulations of single-phase flow
 - backflow through radial clearances
 - pulsations of massflow
- Cavitation simulations
 - blockage effect of cavitation: vapor is displaced in the chambers
 - massflow decreases
- Cavitation model needs further improvements



For more information, visit our stand!